

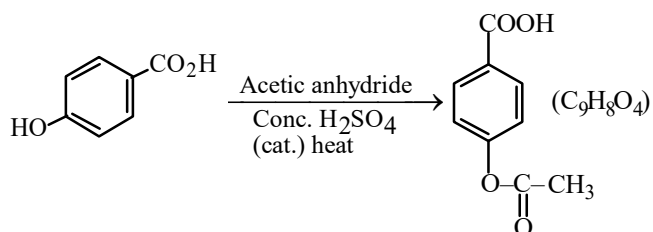
JEE MAIN 2020

FULL TEST-2 SOLUTIONS

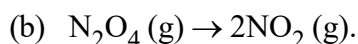
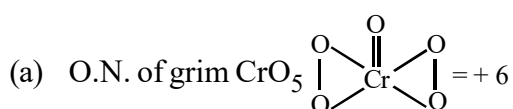
STANDARD ANSWER KEY

Q	1	2	3	4	5	6	7	8	9	10	11
A	1	1	3	2	4	1	2	3	4	4	1
Q	12	13	14	15	16	17	18	19	20	21	22
A	1	2	2	4	1	2	3	1	2	5	6
Q	23	24	25	26	27	28	29	30	31	32	33
A	7	5	2	1	3	3	1	4	2	1	3
Q	34	35	36	37	38	39	40	41	42	43	44
A	1	3	1	4	1	4	4	4	1	2	3
Q	45	46	47	48	49	50	51	52	53	54	55
A	3	5	3	6	4	4	3	1	4	3	2
Q	56	57	58	59	60	61	62	63	64	65	66
A	2	4	1	3	2	3	2	3	1	2	4
Q	67	68	69	70	71	72	73	74	75		
A	3	1	4	3	4	8	1	3	2		

(1) (1).

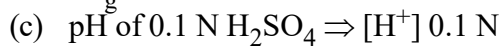


(2) (1).



$$\Delta H = \Delta U + \Delta n_g RT$$

$$\Delta n_g = 2 - 1 \text{ so } \Delta H > \Delta U$$



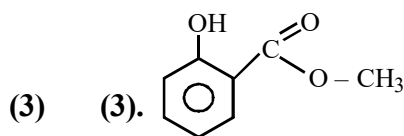
$$\text{pH} = -\log [\text{H}^+] = 10 \text{ g} (10^{-1})$$

$$\text{pH of } 0.1 \text{ N HCl} = [\text{H}^+] = 0.1 \text{ N}$$

$$\text{pH} = \log [\text{H}^+] = -\log (10^{-1}) = (1)$$

(d) $\frac{RT}{F} = \frac{8.314 \times 298}{96500} = 0.256$

$$\frac{2.303RT}{F} = \frac{2.303 \times 8.314 \times 298}{96500} = 0.0591$$



Methyl-2-Hydroxy benzoate.

(4) (2). 1st electron affinity order : $\text{N} < \text{C} < \text{O}$

According to electronic configuration

$$\text{N} = 1s^2 2s^2 2p^3$$

Half-filled orbital are more stable

$$\text{EA, kJ/mole} \begin{pmatrix} \text{C} = 121.77 \\ \text{N} = -6.8 \\ \text{O} = 140 \end{pmatrix}$$

(5) (4). For Lyman : $\bar{\nu}_{\max} = R_H \left(\frac{1}{1^2} - \frac{1}{\infty^2} \right) = R_H$

$$\bar{\nu}_{\min} = R_H \left(\frac{1}{1^2} - \frac{1}{2^2} \right) = \frac{3}{4} R_H$$

$$\Delta \bar{\nu}_{\text{Lyman}} = \frac{R_H}{4}$$

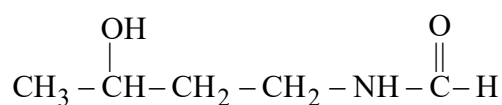
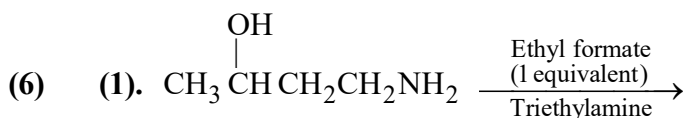
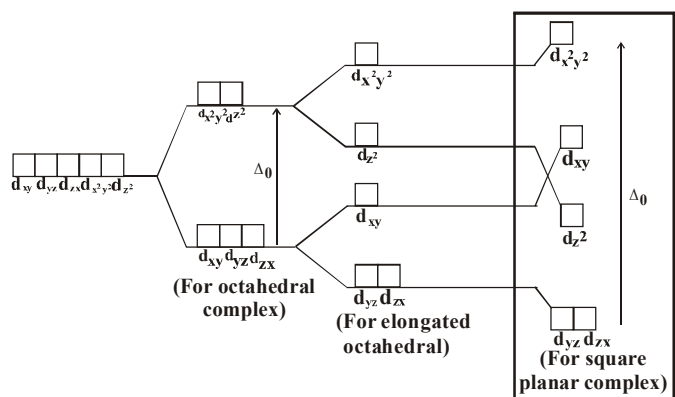
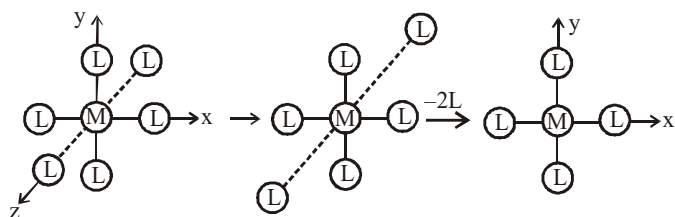
For Balmer

$$\bar{\nu}_{\max} = R_H \left(\frac{1}{2^2} - \frac{1}{\infty^2} \right) = \frac{R_H}{4}$$

$$\bar{v}_{\min} = R_H \left(\frac{1}{2^2} - \frac{1}{3^2} \right) = \frac{5}{36} R_H$$

$$\Delta \bar{v}_{\text{Balmer}} = \frac{R_H}{4} - \frac{5R_H}{36} = \frac{4R_H}{36} = \frac{R_H}{9}$$

$$\frac{\Delta \bar{v}_{\text{Lyman}}}{\Delta \bar{v}_{\text{Balmer}}} = \frac{R_H / 4}{R_H / 9} = \frac{9}{4}$$

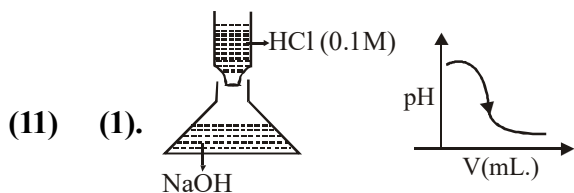


as NH_2 is a better nucleophile than OH .

- (7) (2).
- (1) Zincite is ZnO .
 - (2) Aniline is the forth stabilizer.
 - (3) Zone refining process is not used for refining of 'Ti'.
 - (4) Sodium cyanide is used in the metallurgy of silver.

- (8) (3).
- Gas A and C have same value of 'b' but different value of 'a' so gas having higher value of 'a' have more force of attraction so molecules will be more closer hence occupy less volume.
 - Gas B and D have same value of 'a' but different value of 'b' so gas having lesser value of 'b' will be more compressible.

- (9) (4). $E^\circ_{\text{Red}} \uparrow \Rightarrow$ oxidizing power \uparrow
- (10) (4). High density polythene : Ziegler-Natta catalyst
 Polyacrylonitrile : Peroxide catalyst
 Novolac : Acid or base catalyst
 Nylon 6 : Condensation at high temperature & pressure.

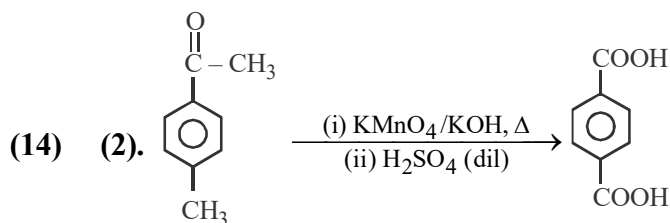


- (12) (1). If both ligands present along z-axis removed from octahedral field and converted into square planar field, then

(13) (2). $y_A = \frac{P_A}{P_{\text{Total}}} = \frac{P_A^0 x_A}{P_A^0 x_A + P_B^0 x_B}$

$$= \frac{7 \times 10^3 \times 0.4}{7 \times 10^3 \times 0.4 + 12 \times 10^3 \times 0.6} = \frac{2.8}{10} = 0.28$$

$y_B = 0.72$

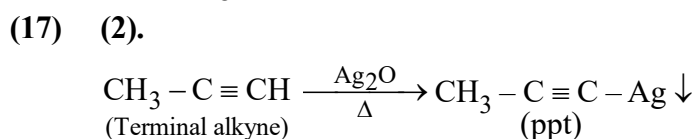


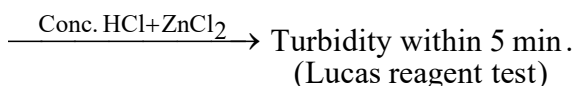
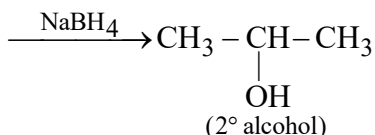
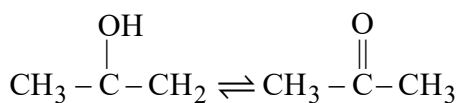
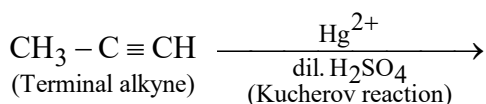
- (15) (4). Catenation is not shown by lead.

- (16) (1). For zero order
 $[A_0] - [A_t] = kt$
 $0.2 - 0.1 = k \times 6$

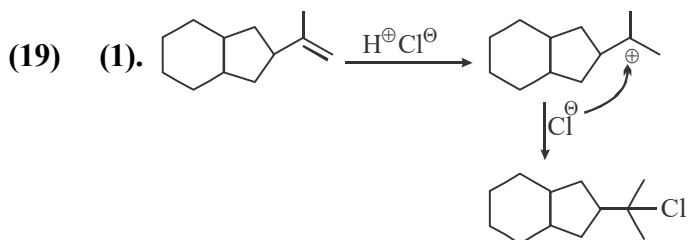
$$k = \frac{1}{60} \text{ M/hr and } 0.5 - 0.2 = \frac{1}{60} \times t$$

$t = 18 \text{ hrs.}$





- (18) (3). Main principle of column chromatography is differential adsorption of the substance on the solid phase.



- (20) (2). $\text{Na}_2\text{CO}_3 \cdot 10\text{H}_2\text{O} \rightarrow$ Solvay process
 $\text{Mg}(\text{HCO}_3)_2 \rightarrow$ Temporary hardness
 $\text{NaOH} \rightarrow$ Castner-kellner cell
 $\text{Ca}_3\text{Al}_2\text{O}_6 \rightarrow$ Portland cement

- (21) 5. $[\text{Pt}(\text{NH}_3)\text{Cl}(\text{H}_2\text{O})\text{Br}]$, $[\text{Cu}(\text{NH}_3)_4]^{2+}$,
 $[\text{Co}(\text{en}_3)]^{3+}$, XeF_4 , XeO_6^{4-} .

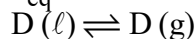
$d_{x^2-y^2}$ orbital involved in dsp^2 & $\text{sp}^3\text{d}^2/\text{d}^2\text{sp}^3$ hybridisation.

- (1) dsp^2 : $[\text{Pt}(\text{NH}_3)\text{Cl}(\text{H}_2\text{O})\text{Br}] \rightarrow$ Square planar
 (2) sp^3d : $\text{SF}_4 \rightarrow$ See-Saw sp^3d
 (3) dsp^2 : $[\text{Cu}(\text{NH}_3)_4]^{2+} \rightarrow$ Square planar
 (4) sp^3d : $[\text{XeO}_3\text{F}_2] \rightarrow$ Trigonal bipyramidal
 (5) sp^3d : $[\text{XeO}_2\text{F}_2] \rightarrow$ See-Saw
 (6) d^2sp^3 : $[\text{Co}(\text{en}_3)]^{3+} \rightarrow$ Octahedral
 (7) dsp^3 : $[\text{Fe}(\text{CO})_5] \rightarrow$ Square pyramidal
 (8) sp^3 : $\text{POCl}_3 \rightarrow$ Tetrahedral
 (9) sp^3d^2 : $\text{XeF}_4 \rightarrow$ Square planar
 (10) sp^3d^2 : $\text{XeO}_6^{4-} \rightarrow$ Square bipyramidal

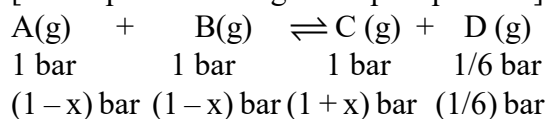
- (22) 6. $\text{A}(\text{g}) + \text{B}(\text{g}) \rightleftharpoons \text{C}(\text{g}) + \text{D}$
 $= \Delta G^\circ_{\text{reaction}}$
 $= (\Delta G^\circ_{\text{fC}} + \Delta G^\circ_{\text{fD}}) - (\Delta G^\circ_{\text{fA}} + \Delta G^\circ_{\text{fB}})$
 $= (-50 \text{ kJ} + 100 \text{ kJ}) - (30 \text{ kJ} + 20 \text{ kJ})$
 $\Delta G^\circ = 0$

$$\Delta G^\circ = -RT \ln k_{\text{eq}}$$

$$k_{\text{eq}} = 1$$



[Partial pressure of D gas = Vapour pressure]



$$K_{\text{eq}} = 1 = \frac{1/6 \times [1+x]}{(1-x)^2}$$

$$1 + x^2 - 2x = \frac{1}{6} + \frac{x}{6}; \quad x^2 - 2x - \frac{x}{6} + \frac{5}{6} = 0$$

$$x^2 - \frac{13x}{6} + \frac{5}{6} = 0$$

$$6x^2 - 13x + 5; \quad x = 1/2$$

$$P_A = 1/2, \quad P_B = 1/2, \quad P_A = 3/2$$

$$a = 1, \quad b = 1, \quad c = 1, \quad d = 3$$

- (23) 7. Molar mass of salt = $120 + 18x$
 Mass of water present in the salt

$$= \frac{18x}{120 + 18x} \times 32\text{g}$$

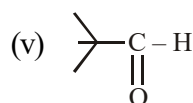
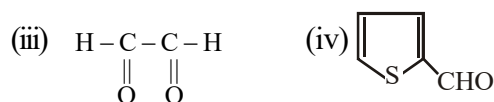
Molality of the solution

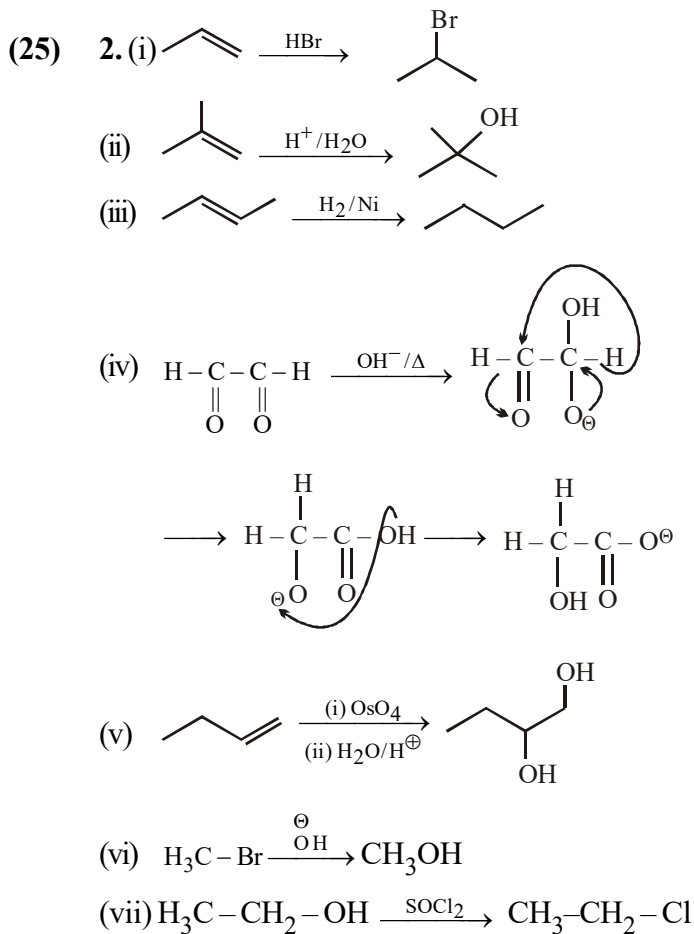
$$= \frac{32}{120 + 18x} \times \left[\frac{1000}{84 + \frac{18 \times 32x}{120 + 18x}} \right] = \frac{4000}{1260 + 261x}$$

$$\Delta T_f = 4.836 = 2 \times 1.86 \times \frac{4000}{1260 + 261x}$$

$$x = 6.9 \approx 7$$

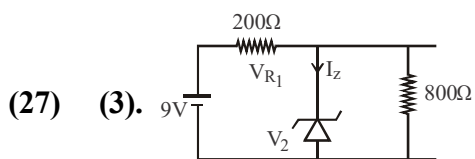
- (24) 5. Compound with α -H absent will give Cannizaro reaction.





(26) (1). $T^2 \propto r^3, \frac{r_E}{r_P} = \left(\frac{T_E}{T_P}\right)^{2/3} = \left(\frac{\omega_P}{\omega_E}\right)^{2/3}$

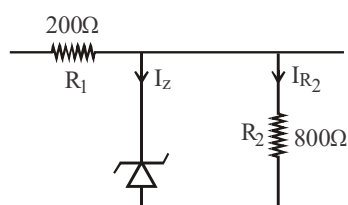
$$\frac{R}{r_P} = (2)^{2/3}; r_P = (2)^{-2/3} R$$



$$9 = V_Z + V_{R_1}; V_Z = 5.6 \text{ V}$$

$$V_{R_1} = 9 - 5.6 = 3.4$$

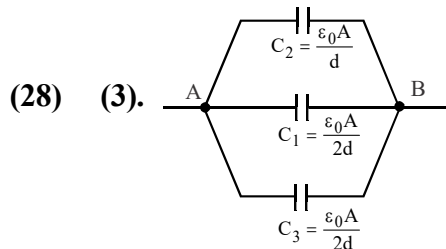
$$I_{R_1} = \frac{V_{R_1}}{R} = \frac{3.4}{200} = 17 \text{ mA}$$



$$V_Z = V_{R_2} = I_{R_2}(R_2)$$

$$\frac{5.6}{800} = I_{R_2}; I_{R_2} = 7 \text{ mA}$$

$$I_Z = (17 - 7) \text{ mA} = 10 \text{ mA}$$



$$C_{eq} = \frac{\epsilon_0 A}{d} + \frac{\epsilon_0 A}{2d} + \frac{\epsilon_0 A}{2d} = \frac{2\epsilon_0 A}{d}$$

(29) (1). $\frac{1}{\lambda} = R \left(\frac{1}{1^2} - \frac{1}{2^2} \right)$

$$\frac{1}{\lambda_1} = R \left(\frac{1}{3^2} - \frac{1}{4^2} \right); \frac{\lambda_1}{\lambda} = \frac{\frac{3}{4}}{\frac{7}{16 \times 9}}$$

$$\lambda_1 = \frac{3}{4} \times \frac{16 \times 9}{7} \lambda = \frac{108}{7} \lambda$$

(30) (4). Magnification is 2
If image is real, $x_1 = 3f/2$
If image is virtual, $x_2 = f/2$

$$\frac{x_1}{x_2} = 3:1$$

(31) (2). $B = \frac{\mu_0 i}{2R} = \frac{\mu_0 q \omega}{2R \times 2\pi}$
 $\Rightarrow q = 3 \times 10^{-5} \text{ C}$

(32) (1). $\beta = \frac{\lambda D}{d}$

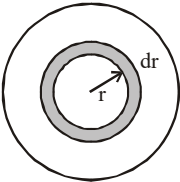
$$\frac{\Delta\beta}{\beta} \times 100 = \frac{\Delta D}{D} \times 100 - \frac{\Delta d}{d} \times 100$$

$$= 0.5 - (-0.3) = 0.8\%$$

Fringe width increases by 0.8%.
(33) (3). The physical size of antenna of receiver and transmitter both inversely proportional to carrier frequency.

(34) (1). $\frac{F}{A} = \text{Stress}$; $\frac{400 \times 4}{\pi d^2} = 379 \times 10^6$
 $d^2 = \frac{1600}{\pi \times 379 \times 10^6} = 1.34 \times 10^{-6}$
 $d = \sqrt{1.34 \times 10^{-6}} = 1.15 \times 10^{-3} \text{ m}$

(35) (3). $I_{\text{Disc}} = \int_0^R (dm) r^2 = \int_0^R (\sigma 2\pi r dr) r^2$
 $I_{\text{Disc}} = \int_0^R (kr^2 2\pi r dr) r^2 = 2\pi k \int_0^R r^5 dr$
 $= 2\pi k \left(\frac{r^6}{6} \right)_0^R = 2\pi k \frac{R^6}{6}$



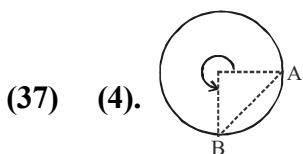
Mass of disc, $M = \int_0^R 2\pi r dr kr^2$
 $= 2\pi k \int_0^R r^3 dr = 2\pi k \left(\frac{r^4}{4} \right)_0^R = 2\pi k \frac{R^4}{4}$

$I_{\text{disc}} = \frac{2}{3} MR^2$

(36) (1). $M = NIA$; $dq = \lambda dx$ & $A = \pi x^2$
 $\int dm = \int (n) \frac{\rho_0 x}{\ell} dx \cdot \pi x^2$

$M = \frac{n\rho_0\pi}{\ell} \int_0^\ell x^3 \cdot dx = \frac{n\rho_0\pi}{\ell} \left[\frac{\ell^4}{4} \right]$

$M = \frac{n\rho_0\pi\ell^3}{4}$



$|\vec{V}| = \frac{R\sqrt{2}}{\left(\frac{3\pi R}{2}\right)} = \frac{2\sqrt{2}v}{3\pi} = \frac{4}{3\pi} \text{ m/s}$

(38) (1). $f = 660 \text{ Hz}$, $v = 330 \text{ m/s}$
 $S_1 \rightarrow v \xrightarrow{u} v \leftarrow S_2$

$f_1 = f \left(\frac{v-u}{v} \right)$; $f_2 = f \left(\frac{v+u}{v} \right)$

$f_2 - f_1 = \frac{f}{v} [v+u - (v-u)]$

$10 = f_2 - f_1 = \frac{f}{v} [2u]$

$u = 2.5 \text{ m/s}$

(39) (4). $\vec{P}_1 = \frac{h}{\lambda_1} \hat{i}$; $\vec{P}_2 = \frac{h}{\lambda_2} \hat{j}$

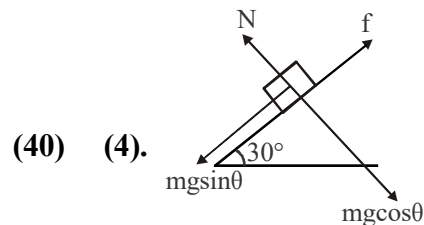
$\vec{P}_1 = \frac{h}{\lambda_1} \hat{i}$ & $\vec{P}_2 = \frac{h}{\lambda_2} \hat{j}$

Using momentum conservation

$\vec{P} = \vec{P}_1 + \vec{P}_2 = \frac{h}{\lambda_1} \hat{i} + \frac{h}{\lambda_2} \hat{j}$

$|\vec{P}| = \sqrt{\left(\frac{h}{\lambda_1}\right)^2 + \left(\frac{h}{\lambda_2}\right)^2}$

$\frac{h}{\lambda} = \sqrt{\left(\frac{h}{\lambda_1}\right)^2 + \left(\frac{h}{\lambda_2}\right)^2}$; $\frac{1}{\lambda^2} = \frac{1}{\lambda_1^2} + \frac{1}{\lambda_2^2}$



Since block is at rest

$N = mg \cos \theta$ & $f = mg \sin \theta$

Force exerted by the surface on the block will

$be = \sqrt{N^2 + f^2} = mg = 80 \text{ N}$

(41) (4). $M = M_0 e^{-\lambda t}$; Given $t = 2 \left(\frac{1}{\lambda} \right)$

$\Rightarrow M = 10e^{-\lambda \left(\frac{2}{\lambda} \right)} = 10 \left(\frac{1}{e} \right)^2$ (e = 2.71)

$\Rightarrow M = 1.35 \text{ g}$

(42) (1). State function $(\Delta U)_{\text{cycle}} = 0$
and (work) = -ve [anticlockwise]

\therefore Using FLOT
 $Q = \Delta U + W$
Also $(Q = -ve)$

(43) (2). Let distance moved by plank = x
 $3Mx = M(\ell - x)$
 $x = \ell / 4$

Distance moved by man = $\ell - \frac{\ell}{4} = \frac{3\ell}{4}$

(44) (3). L.C. = 1 MSD - 1 VSD

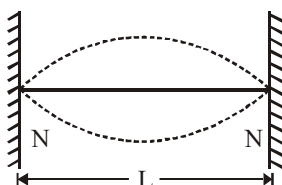
= 1 MSD - $\frac{9}{10}$ MSD

= $\left(1 - \frac{9}{10} \right) \times 1 \text{ MSD}$

= 0.1 \times 0.1 cm
= 0.01 cm

Diameter = MSR + LC \times VSR
= 1.3 + 0.01 \times 2 = 1.3 + 0.02 = 1.32 cm

(45) (3). Here, mass of the wire,
 $M = 30 \text{ g} = 30 \times 10^{-3} \text{ kg}$
Mass per unit length of the wire,
 $\mu = 4 \times 10^{-2} \text{ kg m}^{-1}$



\therefore Length of the wire,

$L = \frac{M}{\mu} = \frac{30 \times 10^{-3} \text{ kg}}{4 \times 10^{-2} \text{ kg m}^{-1}} = 0.75 \text{ m}$

For the fundamental mode $\frac{\lambda}{2} = L$

$\Rightarrow \lambda = 2L = 2 \times 0.75 = 1.5 \text{ m}$
Speed of the transverse wave,
 $v = n \lambda = (50 \text{ s}^{-1}) (1.5 \text{ m}) = 75 \text{ m s}^{-1}$

(46) 5. $\Delta Q = \Delta U + \Delta W \Rightarrow \Delta W = -\Delta U = \frac{f}{2} n R \Delta T$

$147 = \frac{f}{2} \times 8.4 \times 7 \Rightarrow f = \frac{147}{7 \times 4.2} = 5$

(47) 3. Magnification, $m = \frac{-f}{-f + \frac{3f}{2}} = -2$

Taking the direction in the right hand side

$V_{\text{im}} = -m^2 V_{\text{om}}$

$V_{\text{im}} \rightarrow$ velocity of image w.r.t. mirror

$V_{\text{om}} \rightarrow$ velocity of object w.r.t mirror

$\Rightarrow V_{\text{im}} = -4u$

$V_{\text{m}} = \frac{-mu}{m + 2m} = -\frac{u}{3}$

\rightarrow Velocity of platform (minor)

$V_{\text{im}} = V_{\text{i}} - V_{\text{m}}$

$V_{\text{i}} \rightarrow$ velocity of image w.r.t ground

$\Rightarrow V_{\text{i}} = -4u - \frac{u}{3} \Rightarrow V_{\text{i}} = -\frac{13}{3}u$

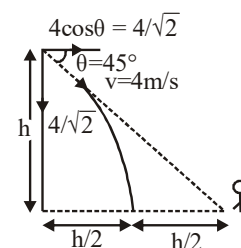
$\Rightarrow V_{\text{i}} = 3 \text{ m/s}$

(48) 6. After a large no. of time, the potential of each capacitor will be equal to the potential of the reservoir.

$\Rightarrow Q_2 = C_2 V$
 $Q_2 = 6\mu\text{C}$

(49) 4. $\frac{4}{\sqrt{2}} \cdot t = \frac{h}{2} \dots\dots (1)$

$h = \left(\frac{4}{\sqrt{2}} \right) \cdot t + \frac{1}{2} g t^2$
 $\dots\dots (2)$



From eq. (1) & (2)

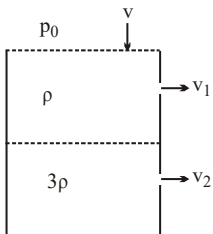
$\frac{h}{2} = \frac{1}{2} g \frac{4^2}{2} = \frac{1}{2} g \left(\frac{h}{4\sqrt{2}} \right)^2$

$h = \frac{16 \times 2}{10} = 3.2 \text{ m}$

(50) 4. $\rho_0 + \frac{\rho gh}{3} + \frac{1}{2}\rho v^2 = p_0 + 0 + \frac{1}{2}\rho v_1^2$

$$v_1 = \sqrt{\frac{2gh}{3}}$$

$$\rho_0 + \frac{3\rho gh}{3} + \rho gh + \frac{1}{2}\rho v^2 = p_0 + 0 + \frac{1}{2}3\rho v_2^2$$



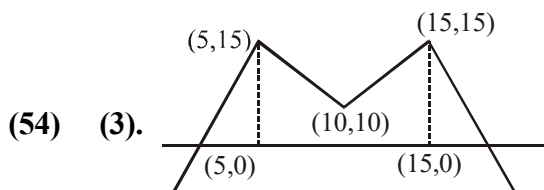
$$v_2 = \sqrt{\frac{4gh}{3}}$$

(51) (3). Equation of required plane is $(3-1)x + (4-2)y + (5-3)z = k$ which passes through $(2, 3, 4)$
 $\Rightarrow k = 9$

\Rightarrow Equation of plane is $x + y + z = 9$

(52) (1). $|A^2| = 25 \Rightarrow |A| = 5$ or -5
 $|A| = 25x = 5$ or $-5 \Rightarrow x = 1/5, -1/5$
 $\Rightarrow |x| = 1/5$

(53) (4). $\int_{\alpha}^{\alpha+1} \frac{(x+\alpha+1) - (x+\alpha)}{(x+\alpha)(x+\alpha+1)} dx$
 $= (\ln|x+\alpha| - \ln|x+\alpha+1|) \Big|_{\alpha}^{\alpha+1}$
 $= \ln \left| \frac{2\alpha+1}{2\alpha+2} \times \frac{2\alpha+1}{2\alpha} \right| = \ln \frac{9}{8}$
 $\Rightarrow \alpha = -2, 1$



$f(x) = 15 - |x - 10|, x \in \mathbb{R}$
 $f(f(x)) = 15 - |f(x) - 10|$
 $= 15 - |15 - |x - 10| - 10|$
 $= 15 - |5 - |x - 10||$
 $x = 5, 10, 15$ are points of non differentiability

Aliter :

At $x = 10$ $f(x)$ is non differentiable
 also, when $15 - |x - 10| = 10$

$\Rightarrow x = 5, 15$

\therefore Non-differentiability points are $\{5, 10, 15\}$

(55) (2). If $AB = AC \Rightarrow \angle ABC = \angle ACB$

$\Rightarrow \tan(\angle ABC) = \tan(\angle ACB)$

If let slope of AC is m

$$\therefore \left| \frac{m + \frac{1}{4}}{1 - \frac{m}{4}} \right| = \left| \frac{-\frac{1}{4} - 1}{1 - \frac{1}{4}} \right|$$

$$\Rightarrow m = \frac{-23}{7}, 1 \text{ (rejected)}$$

\therefore Equation of line is $23x + 7y + 3 = 0$

(56) (2). $\lim_{x \rightarrow 0} \frac{\left(\frac{\sin^2 x}{x^2} \right) (\sqrt{2} + \sqrt{1 + \cos x})}{\left(\frac{1 - \cos x}{x^2} \right)}$

$$= \frac{(1)^2 \cdot (2\sqrt{2})}{1/2} = 4\sqrt{2}$$

(57) (4).

(1) $(p \vee q) \wedge (\sim p \vee \sim q)$
 $\equiv (p \vee q) \wedge \sim(p \wedge q)$
 \rightarrow Not tautology (Take both p and q as T)

(2) $(p \wedge q) \vee (p \wedge \sim q)$
 $\equiv p \wedge (q \vee \sim q) \equiv p \wedge t \equiv p$

(3) $(p \vee q) \wedge (p \vee \sim q)$
 $\equiv p \vee (q \wedge \sim q) \equiv p \vee c \equiv p$

(4) $(p \vee q) \vee (p \vee \sim q)$
 $\equiv p \vee (q \vee \sim q) \equiv p \vee t \equiv t$

(58) (1). $\frac{34+x}{2} = 35 \Rightarrow x = 36$

$$42 = \frac{10 + 22 + 26 + 29 + 34 + 36 + 42 + 67 + 70 + y}{10}$$

$$420 - 336 = y \Rightarrow y = 84$$

$$\frac{y}{x} = \frac{84}{36} = \frac{7}{3}$$

(59) (3). $R_1 \rightarrow R_1 - R_2$

$$\begin{vmatrix} 1 & -1 & 0 \\ \cos^2 \theta & 1 + \sin^2 \theta & 4 \cos 6\theta \\ \cos^2 \theta & \sin^2 \theta & 1 + 4 \cos 6\theta \end{vmatrix} = 0$$

$$R_2 \rightarrow R_2 - R_3$$

$$\begin{vmatrix} 1 & -1 & 0 \\ 0 & 1 & -1 \\ \cos^2 \theta & \sin^2 \theta & 1 + 4 \cos 6\theta \end{vmatrix} = 0$$

$$\Rightarrow (1 + 4 \cos 6\theta) + \sin^2 \theta + 1 (\cos^2 \theta) = 0$$

$$1 + 2 \cos 6\theta = 0 \Rightarrow \cos 6\theta = -1/2$$

$$6\theta = \frac{2\pi}{3} \Rightarrow \theta = \frac{\pi}{9}$$

(60) (2). $\frac{dy}{dx} = \frac{b^2 x}{a^2 y}$

$$\left. -\frac{dx}{dy} \right]_{(4,3)} = -\frac{3a^2}{4b^2} = \frac{3-0}{4-16}$$

$$\frac{a^2}{b^2} = \frac{1}{3} \Rightarrow \frac{b^2}{a^2} = 3$$

$$e = \sqrt{\frac{1+b^2}{a^2}} = \sqrt{1+3} = 2$$

(61) (3). Given $y^2 = 4x$... (1)
and $x^2 + y^2 = 5$... (2)

By (1) and (2)
 $\Rightarrow x = 1$ and $y = 2$
Equation of tangent at (1, 2) to $y^2 = 4x$
is $y = x + 1$

(62) (2). $T_4 = T_{3+1} = \binom{6}{3} \left(\frac{2}{x}\right)^3 \cdot (x^{\log_8 x})^3$

$$20 \times 8^7 = \frac{160}{x^3} \cdot x^{3 \log_8 x}$$

$$8^6 = x^{\log_2 x - 3}$$

$$2^{18} = x^{\log_2 x - 3}$$

$$\Rightarrow 18 = (\log_2 x - 3) (\log_2 x)$$

Let $\log_2 x = t$

$$\Rightarrow t^2 - 3t - 18 = 0$$

$$\Rightarrow (t - 6) (t + 3) = 0$$

$$\Rightarrow t = 6, -3$$

$$\log_2 x = 6 \Rightarrow x = 2^6 = 8^2$$

$$\log_2 x = -3 \Rightarrow x = 2^{-3} = 8^{-1}$$

(63) (3). Probability that no student solve the problem is

$$\left(1 - \frac{1}{2}\right) \left(1 - \frac{1}{3}\right) \left(1 - \frac{1}{4}\right) \left(1 - \frac{1}{5}\right) = \frac{1}{2} \times \frac{2}{3} \times \frac{3}{4} \times \frac{4}{5} = \frac{1}{5}$$

Probability that the problem will be solved by

at least one student is equal to $1 - \frac{1}{5} = \frac{4}{5}$.

(64) (1). ${}^6C_2 \times {}^6C_4 + {}^6C_3 \times {}^6C_3 + {}^6C_4 \times {}^6C_2$
 $= (12)^2 + (20)^2 + (15)^2$
 $= 225 + 400 + 225 = 850$

(65) (2). S_A = sum of numbers between 100 & 200 which are divisible by 7.
 $\Rightarrow S_A = 105 + 112 + \dots + 196$

$$S_A = \frac{14}{2} [105 + 196] = 2107$$

S_B = Sum of numbers between 100 & 200 which are divisible by 13.

$$S_B = 104 + 117 + \dots + 195$$

$$= \frac{8}{2} [104 + 195] = 1196$$

S_C = Sum of numbers between 100 & 200 which are divisible by both 7 & 13.

$$S_C = 182$$

$$\Rightarrow \text{H.C.F. } (91, n) > 1 = S_A + S_B - S_C = 3121$$

(66) (4). $\cos 2\theta = \frac{1 - \tan^2 \theta}{1 + \tan^2 \theta}$

$$\int \cos \left(2 \left(\tan^{-1} \sqrt{\frac{1-x}{1+x}} \right) \right) dx = \int \frac{1 - \left(\frac{1-x}{1+x} \right)}{1 + \frac{1-x}{1+x}} dx$$

$$= \int x dx = \frac{x^2}{2} + c$$

$y = \frac{x^2}{2} + c$ are family of parabolas.

(67) (3). $a < b < c$ are in A.P.
 $\angle C = 2 \angle A$ (Given)
 $\Rightarrow \sin C = \sin 2A$
 $\Rightarrow \sin C = 2 \sin A \cdot \cos A$
 $\Rightarrow \frac{\sin C}{\sin A} = 2 \cos A$

$$\Rightarrow \frac{c}{a} = 2 \frac{b^2 + c^2 - a^2}{2bc}$$

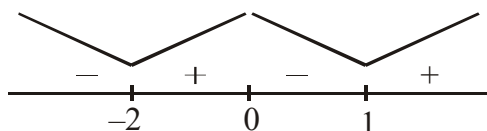
Put $a = b - \lambda, c = b + \lambda, \lambda > 0$

$$\Rightarrow \lambda = \frac{b}{5}$$

$$\Rightarrow a = b - \frac{b}{5} = \frac{4}{5}b, c = b + \frac{b}{5} = \frac{6b}{5}$$

\Rightarrow Required ratio = 4 : 5 : 6

(68) (1). $f(x) = 9x^4 + 12x^3 - 36x^2 + 25$
 $f'(x) = 36x^3 + 36x^2 - 72x$
 $= 36x(x^2 + x - 2)$
 $= 36x(x - 1)(x + 2)$



Points of minima = $\{-2, 1\} = S_1$

Point of maxima = $\{0\} = S_2$

(69) (4). $\bar{x} = \frac{6(2\hat{i} - 2\hat{j} + \hat{k})}{3}, \bar{y} = \frac{\sqrt{3}(\hat{i} + \hat{j} - \hat{k})}{\sqrt{3}}$

$$|\bar{x} + 2\bar{y}| = |6\hat{i} - 2\hat{j}| = \sqrt{40} = 2\sqrt{10}$$

(70) (3). R is reflexive if it contains (1, 1) (2, 2) (3, 3)

$\therefore (1, 2) \in R, (2, 3) \in R$

\therefore R is symmetric if (2, 1), (3, 2) \in R

Now, $R = \{(1, 1), (2, 2), (3, 3), (2, 1), (3, 2), (2, 3), (1, 2)\}$

R will be transitive if (3, 1); (1, 3) \in R.

Thus, R becomes an equivalence relation by adding (1, 1) (2, 2) (3, 3) (2, 1), (3, 2),

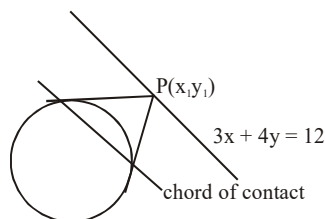
(1, 3), (1, 2). Hence, the total number of ordered pairs is 7.

(71) 4. Let $P(x_1, y_1)$ be a point on the line

$$3x + 4y = 12.$$

Equation of variable chord of contact of

$P(x_1, y_1)$ wrt circle $x^2 + y^2 = 4$ is



$$xx_1 + yy_1 - 4 = 0 \dots (1)$$

$$\text{Also } 3x_1 + 4y_1 - 12 = 0$$

$$x_1 + \frac{4}{3}y_1 - 4 = 0 \dots (2)$$

Comparing (1) & (2), $x = 1, y = 4/3$

\therefore Variable chord of contact always passes through (1, 4/3).

(72) 8. Let $n(A)$ = number of students opted Mathematics = 70,

$n(B)$ = number of students opted Physics = 46,

$n(C)$ = number of students opted Chemistry = 28,

$n(A \cap B) = 23, n(B \cap C) = 9,$

$n(A \cap C) = 14, n(A \cap B \cap C) = 4,$

Now $n(A \cup B \cup C)$

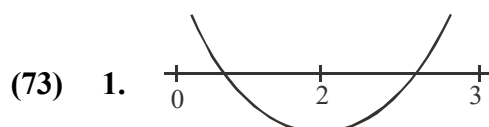
$$= n(A) + n(B) + n(C) - n(A \cap B)$$

$$- n(B \cap C) - n(A \cap C) + n(A \cap B \cap C)$$

$$= 70 + 46 + 28 - 23 - 9 - 14 + 4 = 102$$

Number of students not opted for any course

$$= \text{Total} - n(A \cup B \cup C) = 140 - 102 = 38$$



Let $f(x) = (c - 5)x^2 - 2cx + c - 4$

$$\therefore f(0)f(2) < 0 \dots (1)$$

$$\& f(2)f(3) < 0 \dots (2)$$

From (1) & (2)

$$(c - 4)(c - 24) < 0$$

$$\& (c - 24)(4c - 49) < 0$$

$$\Rightarrow \frac{49}{4} < c < 49$$

$$\therefore s = \{13, 14, 15, \dots, 23\}$$

Number of elements in set S = 11

(74) 3. $\cot \left(\sum_{n=1}^{19} \cot^{-1}(1 + n(n+1)) \right)$

$$= \cot \left(\sum_{n=1}^{19} \cot^{-1}(n^2 + n + 1) \right)$$

$$= \cot \left(\sum_{n=1}^{19} \tan^{-1} \frac{1}{1 + n(n+1)} \right)$$

$$= \sum_{n=1}^{19} (\tan^{-1}(n+1) - \tan^{-1} n)$$

$$= \cot(\tan^{-1} 20 - \tan^{-1} 1) = \frac{\cot A \cot \beta + 1}{\cot \beta - \cot A}$$

(Where $\tan A = 20$, $\tan B = 1$)

$$= \frac{1\left(\frac{1}{20}\right) + 1}{1 - \frac{1}{20}} = \frac{21}{19}$$

(75) 2. $\frac{dy}{dx} + \left(\frac{2x+1}{x}\right)y = e^{-2x}$,

$$\text{I.F.} = e^{\int \left(\frac{2x+1}{x}\right) dx} = e^{\int \left(2 + \frac{1}{x}\right) dx}$$

$$= e^{2x + \ln x} = e^{2x} \cdot x$$

$$y(xe^{2x}) = \int e^{-2x} \cdot x e^{2x} + C$$

$$\Rightarrow xye^{2x} = \int x dx + C$$

$$\Rightarrow 2xye^{2x} = x^2 + 2C$$

It passes through $\left(1, \frac{1}{2}e^{-2}\right)$ we get $C = 0$

$$y = \frac{xe^{-2x}}{2}$$

$$\frac{dy}{dx} = \frac{1}{2}e^{-2x}(-2x+1)$$

$\Rightarrow f(x)$ is decreasing in $(1/2, 1)$.